### 參考題

# (注意:僅供參考,比賽時需加入更多說明及討論)

Steam enters a turbine steadily at 7 MPa and 600 °C with a velocity of 60 m/s and leaves at 25 kPa with a quality of 95 percent. A heat loss of 20 kJ/kg occurs during the process. The inlet area of the turbine is  $150 \text{ cm}^2$ , and the exit area is  $1400 \text{ cm}^2$ . (a) Determine the mass flow rate of the steam, the exit velocity, and the power output.  $(b)$  Investigate the effects of turbine exit area and turbine exit pressure on the exit velocity and power output of the turbine. Let the exit pressure vary from 10 to 50 kPa (with the same quality), and the exit area to vary from 1000 to 3000 cm2 . Plot the exit velocity and the power outlet against the exit pressure for the exit areas of 1000, 2000, and 3000  $\text{cm}^2$ , and discuss the results.

#### (*a*)

*Assumptions* **1** This is a steady-flow process since there is no change with time. **2** Potential energy changes are negligible.

*Properties* From the steam tables (Tables A-4 through 6)

$$
P_1 = 7 \text{ MPa} \mid \nu_1 = 0.05567 \text{ m}^3/\text{kg}
$$
  
T\_1 = 600°C  $\int h_1 = 3650.6 \text{ kJ/kg}$ 

and

 $(0.95)(6.2034 - 0.00102)$ 271.96 + (0.95)(2345.5) = 2500.2 kJ/kg  $0.00102 + (0.95)(6.2034 - 0.00102) = 5.8933 \text{ m}^3/\text{kg}$ 0.95 25 kPa  $2 - n_f + \lambda_2$  $\mathbf{z}_2 = \mathbf{v}_f + x_2 \mathbf{v}_{fg} = 0.00102 + (0.95)(6.2034 - 0.00102) = 5.8933 \text{ m}^3$ 2 2  $= h_f + x_2 h_{f_p} = 271.96 + (0.95)(2345.5) =$  $=$   $v_f + x_2 v_{fo} = 0.00102 + (0.95)(6.2034 - 0.00102)$ J  $\left\{ \right.$  $\overline{1}$ = =  $f^+$  <sup>+</sup>  $\lambda$ <sub>2</sub> $n$ <sub>*fg*</sub>  $f^+$ <sup>+</sup>  $\lambda_2$  $\boldsymbol{\nu}_{fg}$  $h_2 = h_f + x_2 h$ *x x*  $P_2 = 25$  kPa  $\mathbf{v}_2 = \mathbf{v}_1 + x_2 \mathbf{v}$ 

*Analysis* The mass flow rate of the steam is

$$
\dot{m} = \frac{1}{v_1} V_1 A_1 = \frac{1}{0.05567 \text{ m}^3/\text{kg}} (60 \text{ m/s})(0.015 \text{ m}^2) = 16.17 \text{ kg/s}
$$

There is only one inlet and one exit, and thus  $m_1 = m_2 = m$ . Then the exit velocity is determined from

$$
\dot{m} = \frac{1}{v_2} V_2 A_2 \longrightarrow V_2 = \frac{\dot{m} v_2}{A_2} = \frac{(16.17 \text{ kg/s})(5.8933 \text{ m}^3/\text{kg})}{0.14 \text{ m}^2} = 680.6 \text{ m/s}
$$

We take the turbine as the system, which is a control volume since mass crosses the boundary. The energy balance for this steady-flow system can be expressed in the rate form as

$$
\underbrace{\dot{E}_{\text{in}} - \dot{E}_{\text{out}}}_{\text{byte at, work, and mass}} = \underbrace{\Delta \dot{E}_{\text{system}}^{\text{70 (steady)}}}_{\text{Rate of change in internal, kinetic, potential, etc. energies}} = 0
$$
\n
$$
\dot{E}_{\text{in}} = \dot{E}_{\text{out}}
$$



$$
\dot{m}(h_1 + V_1^2 / 2) = \dot{W}_{\text{out}} + \dot{Q}_{\text{out}} + \dot{m}(h_2 + V_2^2 / 2) \text{ (since } \Delta \text{pe} \approx 0)
$$

$$
\dot{W}_{\text{out}} = -\dot{Q}_{\text{out}} - \dot{m} \left( h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} \right)
$$

Then the power output of the turbine is determined by substituting to be

$$
\dot{W}_{\text{out}} = -(16.17 \times 20) \text{ kJ/s} - (16.17 \text{ kg/s}) \left( 2500.2 - 3650.6 + \frac{(680.6 \text{ m/s})^2 - (60 \text{ m/s})^2}{2} \left( \frac{1 \text{ kJ/kg}}{1000 \text{ m}^2/\text{s}^2} \right) \right)
$$
  
= **14,560 kW**

#### EES

A[1]=150 [cm^2] T[1]=600 [C] P[1]=7000 [kPa] Vel[1]= 60 [m/s] A[2]=1400 [cm^2] P[2]=25 [kPa] q out =  $20$  [kJ/kg] m\_dot =  $A[1]^*$ convert(cm<sup>2</sup>, m<sup>2</sup>)\*Vel[1]/v[1] v[1]=volume(steam\_iapws, T=T[1], P=P[1]) "specific volume of steam at state 1" Vel[2]=m\_dot\*v[2]/(A[2]\*Convert(cm^2, m^2)) v[2]=volume(steam\_iapws, x=0.95, P=P[2]) "specific volume of steam at state 2" T[2]=temperature(steam\_iapws, P=P[2], v=v[2]) "not required, but good to know"

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"Conservation of Energy for steady-flow: 
Ein_dot - Eout_dot = DeltaE_dot - For steady-flow, DeltaE_dot = 0"DELTAE_dot=0
"For the turbine as the control volume, neglecting the PE of each flow steam:"
E_dot_in=E_dot_out 
h[1]=enthalpy(steam_iapws,T=T[1], P=P[1]) 
E_dot_in=m_dot*(h[1]+ Vel[1]^2/2*convert(J, kJ) ) 
h[2]=enthalpy(steam_iapws, x=0.95, P=P[2]) 
E_dot_out=m_dot*(h[2]+ Vel[2]^2/2*convert(J, kJ)) + m_dot *q_out+ W_dot_out 
Power=W_dot_out*Convert(kW, MW) 
Q_dot_out=m_dot*q_out
```


## (b)

*Analysis* The problem is solved using EES, and the results are tabulated and plotted below.

Fluid\$='Steam\_IAPWS'

A[1]=150 [cm^2] T[1]=550 [C] P[1]=10000 [kPa] Vel[1]= 60 [m/s] A[2]=1400 [cm^2] P[2]=25 [kPa] q  $out = 30$  [kJ/kg] m\_dot =  $A[1]^*$ Vel[1]/v[1]\*convert(cm^2,m^2) v[1]=volume(Fluid\$, T=T[1], P=P[1]) "specific volume of steam at state 1" Vel[2]=m\_dot\*v[2]/(A[2]\*convert(cm^2,m^2)) v[2]=volume(Fluid\$, x=0.95, P=P[2]) "specific volume of steam at state 2" T[2]=temperature(Fluid\$, P=P[2], v=v[2]) "[C]" "not required, but good to know"

"[conservation of Energy for steady-flow:"

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"Ein_dot - Eout_dot = DeltaE_dot" "For steady-flow, DeltaE_dot = 0"
```
DELTAE\_dot=0 "[kW]"

"For the turbine as the control volume, neglecting the PE of each flow steam:"

E\_dot\_in=E\_dot\_out

h[1]=enthalpy(Fluid\$,T=T[1], P=P[1])

E\_dot\_in=m\_dot\*(h[1]+ Vel[1]^2/2\*Convert(m^2/s^2, kJ/kg))

h[2]=enthalpy(Fluid\$,x=0.95, P=P[2])

E\_dot\_out=m\_dot\*(h[2]+ Vel[2]^2/2\*Convert(m^2/s^2, kJ/kg))+ m\_dot \*q\_out+ W\_dot\_out

Power=W\_dot\_out

Q dot out=m\_dot\*q\_out



Table values are for A[2]=1000 [cm^2]



